



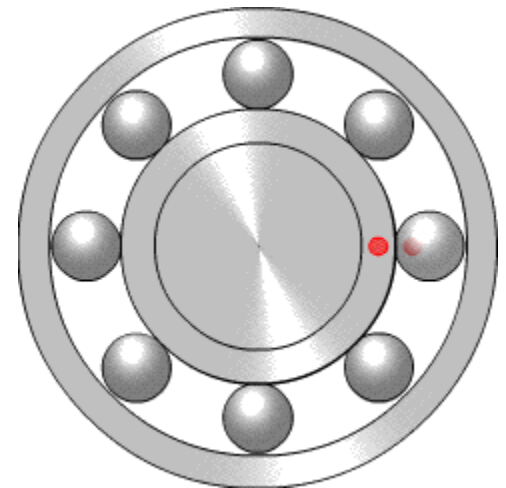
# Friction

## Chapter 8



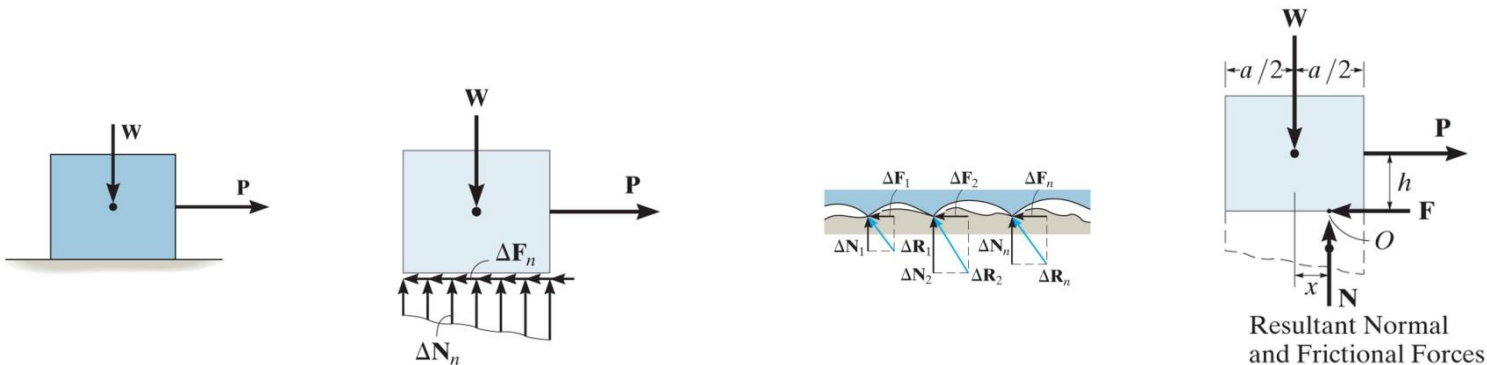
# Overview

- Dry Friction
- Wedges
- Flatbelts
- Screws
- Bearings
- Rolling Resistance



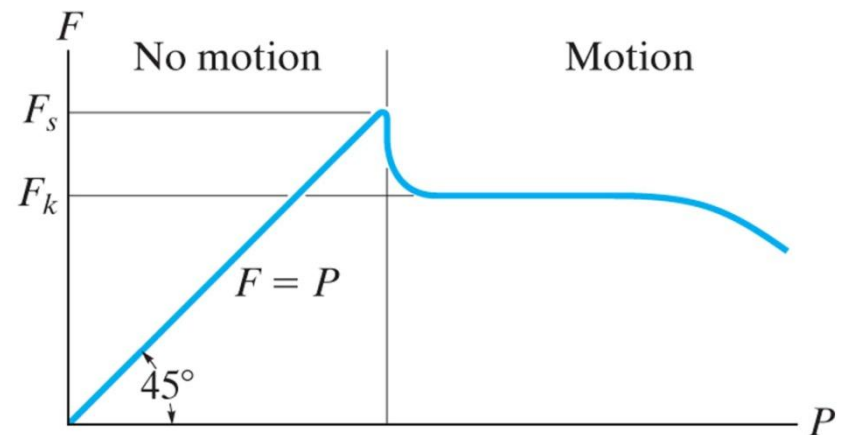
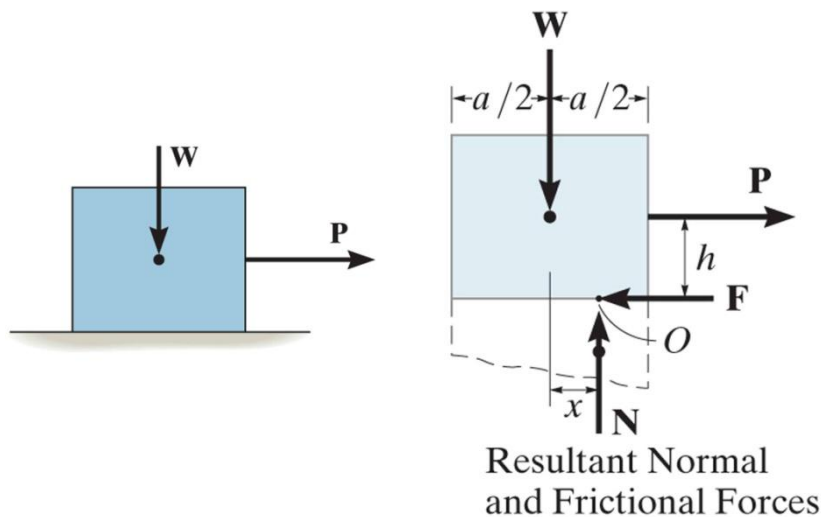
# Dry Friction

- Friction is defined as a force of resistance acting on a body which prevents slipping of the body relative to a second body
- Empirical evidence shows that frictional forces act tangent to the contacting surface in a direction opposing the relative motion or tendency for motion.
- Equilibrium:  $F = P$ ,  $N = W$ , and  $W \cdot x = P \cdot h$ .



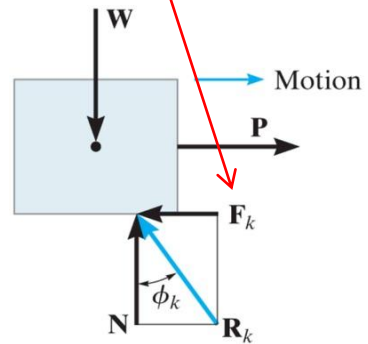
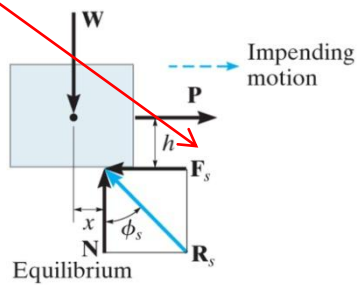
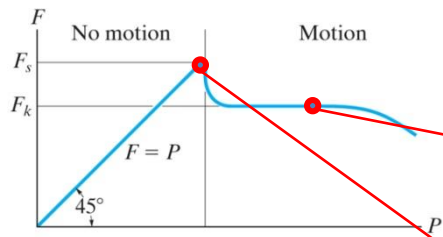
# Dry Friction

- Assume that tipping does not occur (i.e., “h” is small or “a” is large).
- As we gradually increase the magnitude of the force  $P$ , the friction force  $F$  varies with  $P$ ,



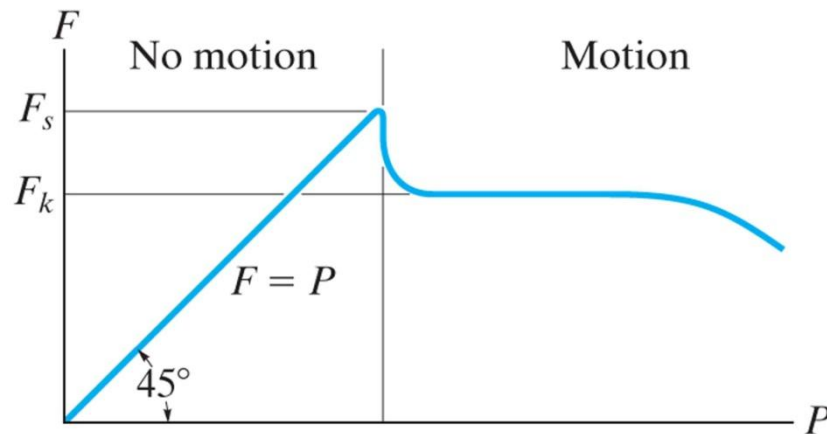
# Dry Friction

- The *maximum friction force* is attained just before the block begins to move (a situation that is called “impending motion”).
- The value of the force is found using  $F_s = \mu_s N$ , where  $\mu_s$  is called the coefficient of static friction.  $\mu_s$  depends on the two materials in contact.
- Once the block begins to move, the frictional force typically drops and is given by  $F_k = \mu_k N$ . The value of  $\mu_k$  is the coefficient of kinetic friction and is less than  $\mu_s$ .



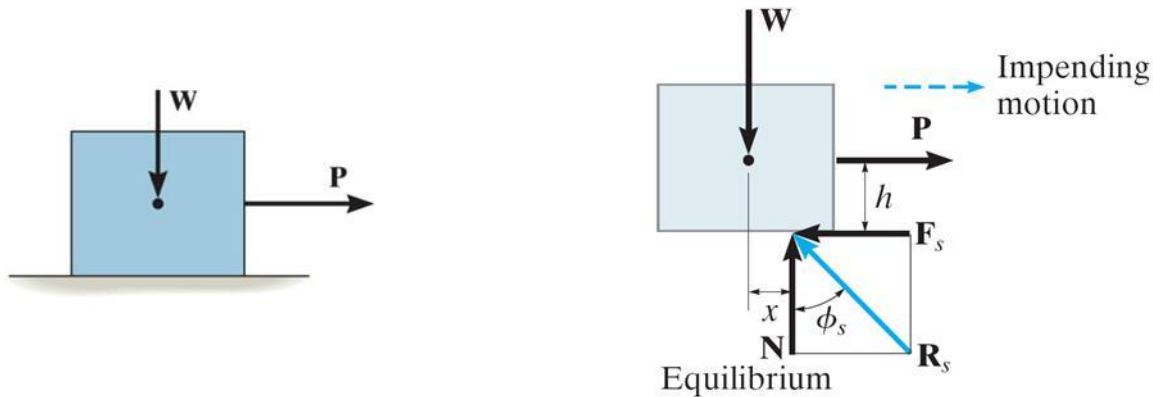
# Dry Friction

- It is important to note that the friction force may be less than the maximum friction force.
- If the object is not moving, don't assume the friction force is at its max. value of  $F_s = \mu_s N$  unless you are told or know motion is impending



# Determining $\mu_s$

- on the verge of sliding, the block just begins to slip, the maximum friction force is  $F_s = \mu_s N$
- Thus,  $N$  and  $F_s$  combine to create a resultant  $R_s$

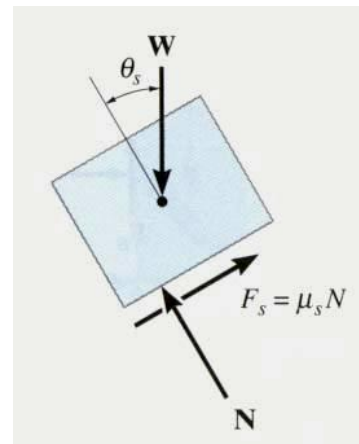
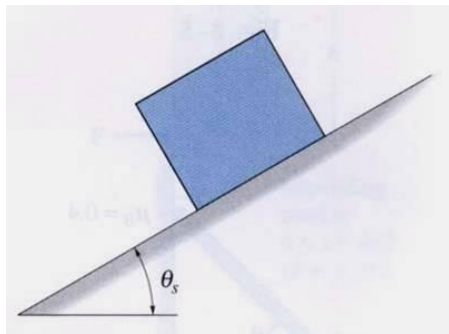


- From the figure,  
$$\tan \phi_s = ( F_s / N ) = ( \mu_s N / N ) = \mu_s$$



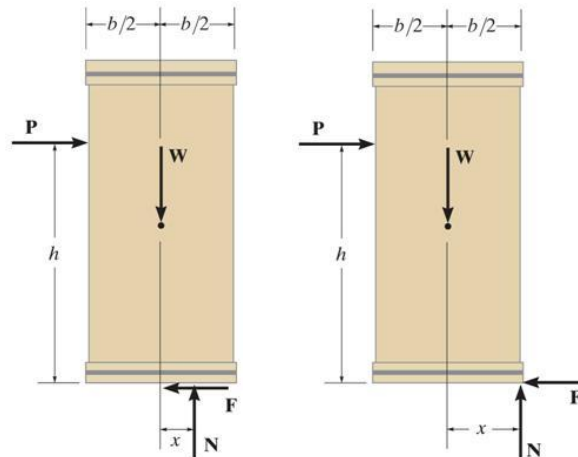
# Determining $\mu_s$ - Inclined Plane

- Analysis of the block just before it begins to move gives (using  $F_s = \mu_s N$ ):
- $\nearrow + \sum F_y = N - W \cos \theta_s = 0$
- $\nearrow + \sum F_x = \mu_s N - W \sin \theta_s = 0$
- $\mu_s = (W \sin \theta_s) / (W \cos \theta_s) = \tan \theta_s$



# Impending Tipping Versus Slipping

- how can we determine if the block will slide or tip first?
- In this case, we have four unknowns ( $F$ ,  $N$ ,  $x$ , and  $P$ ) and only three E-of-E.
- we have to make an assumption to give us another equation (the friction equation!). Then we can solve for the unknowns
- Finally, we need to check if our assumption was correct.



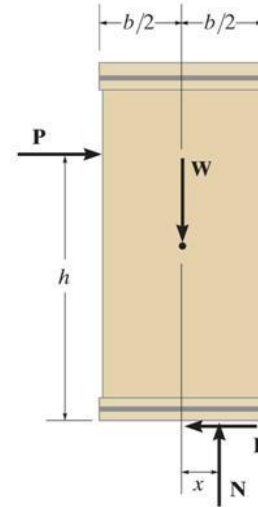
# Impending Tipping Versus Slipping

- Assumption: Slipping occurs

Known:  $F = \mu_s N$

Solve for:  $x$ ,  $P$ , and  $N$

Check:  $0 \leq x \leq b/2$

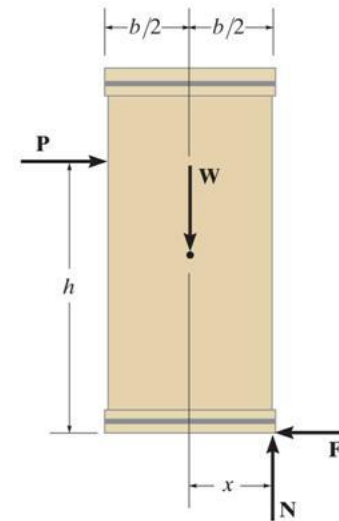


- Assumption: Tipping occurs

Known:  $x = b/2$

Solve for:  $P$ ,  $N$ , and  $F$

Check:  $F \leq \mu_s N$





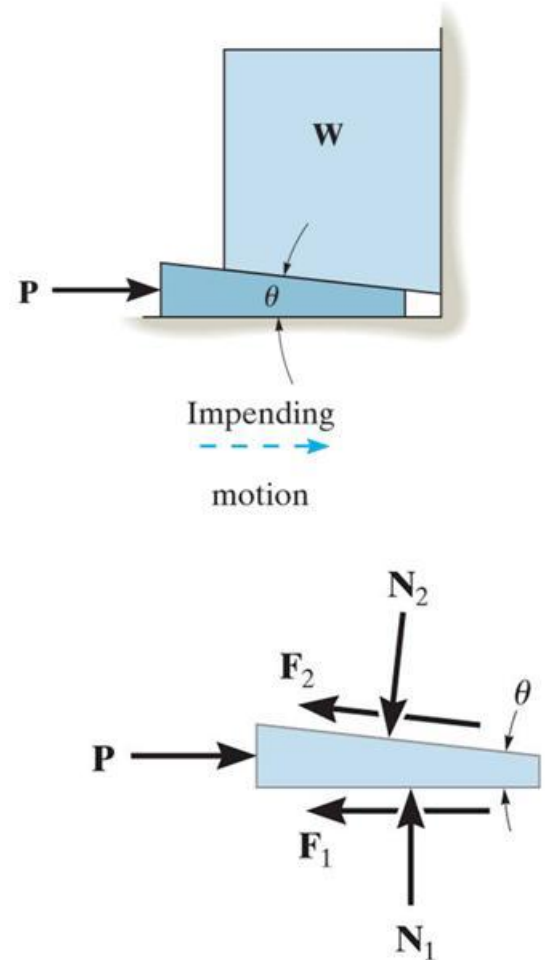
# WEDGES AND FRICTIONAL FORCES ON FLAT BELTS

- Wedges are used to adjust the elevation or provide stability for heavy objects
- Belt drives are commonly used for transmitting the torque developed by a motor to a wheel attached to a pump, fan or blower.



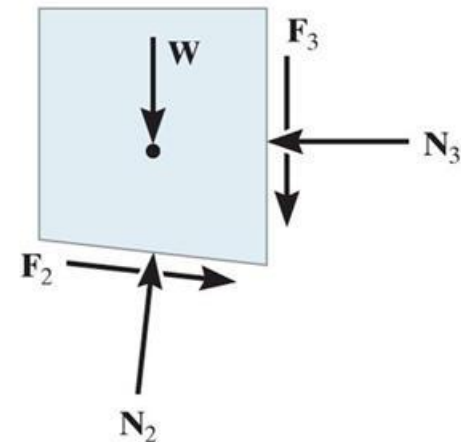
# Analysis of a Wedge

- A wedge is a *simple machine* in which a small force  $P$  is used to lift a large weight  $W$
- First we draw the free body diagram of the wedge, noting that
  - 1) the friction forces are always in the *direction opposite to the motion*,
  - 2) the friction forces are along the contacting surfaces; and,
  - 3) the normal forces are perpendicular to the contacting surfaces



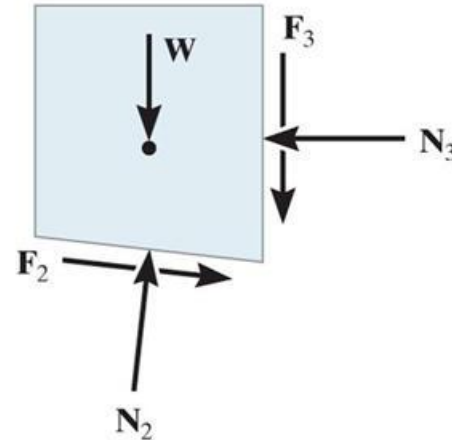
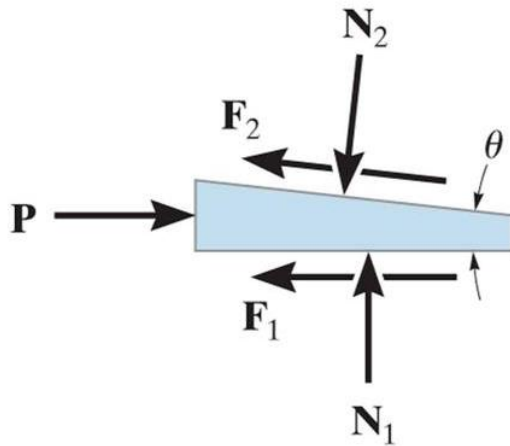
# Analysis of a Wedge

- Next, we look at the object on top of the wedge noting
  - 1) *at the contacting surfaces between the wedge and the object the forces are equal in magnitude and opposite in direction to those on the wedge; and,*
  - 2) all other forces acting on the object should be shown.
  - 3)  $\sum F_x = 0$  and  $\sum F_y = 0$ , for the wedge and the object  
Also, for *the impending motion* frictional equation,  $F = \mu_s N$ .



# Analysis of a Wedge

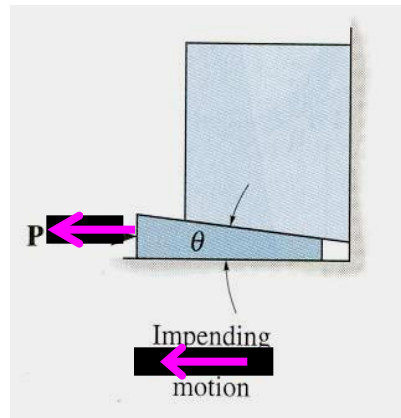
- Start by analyzing the free body diagram in which the number of unknowns are less than or equal to the number of equations of equilibrium and frictional equations





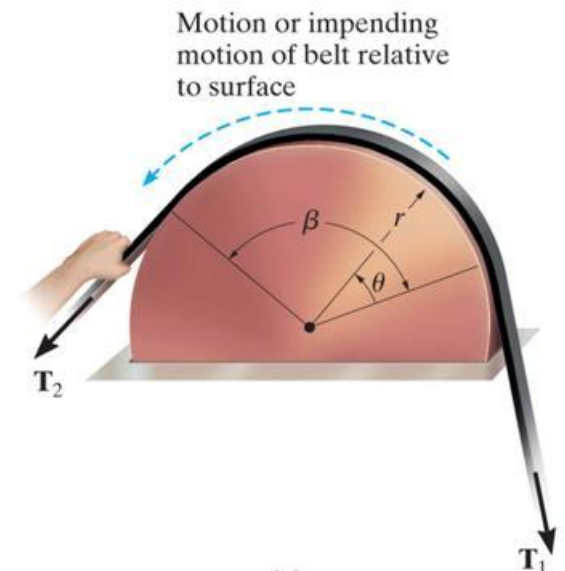
# Analysis of a Wedge

- If the object is to be lowered, then the wedge needs to be pulled out.
- If the value of the force  $P$  needed to remove the wedge is positive, then the wedge is *self-locking*, i.e., it will not come out on its own.



# Analysis of Flat Belt

- Consider a flat belt passing over a fixed curved surface with the total angle of contact equal to  $\beta$  (in radians)
- If the belt slips or is just about to slip, then  $T_2$  must be larger than  $T_1$  plus the motion resisting friction forces. Hence,  $T_2$  must be greater than  $T_1$ .



# Analysis of Flat Belt

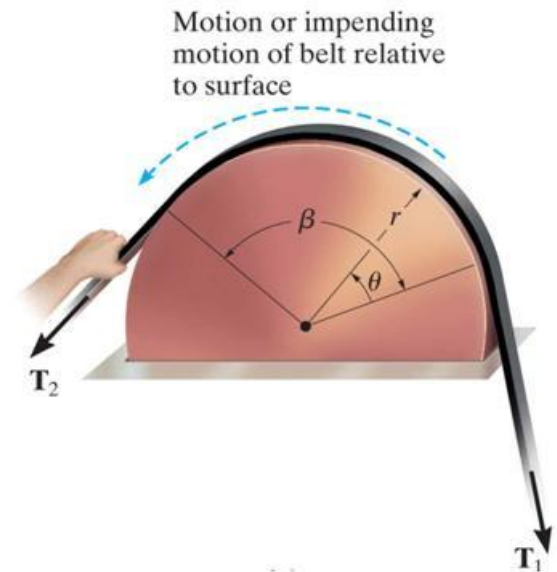
- It can be shown that

$$T_2 = T_1 e^{\mu \beta}$$

where  $\mu$  is the coefficient of static friction between the belt and the surface. [see text for proof]

- Remember to use radians when using this formula!!

- 





# Analysis of Screws



- Screws are used as fasteners or to transmit power or motion from one machine part to another
- Screws can be classified by the *thread*. E.g. *square-threaded screw*, *V-thread*
- A screw is considered a cylinder called a *barrel* or *shaft*, with the *thread* wrapped around it.



fig08\_17a.jpg

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# Analysis of Screws

- If we unwind the thread by one revolution, the slope or *lead angle* is given by

$$\theta = \tan^{-1} \left( \frac{l}{2\pi r} \right)$$

- $l$  is called the *lead* of the screw, and is the distance advanced by turning the screw one revolution

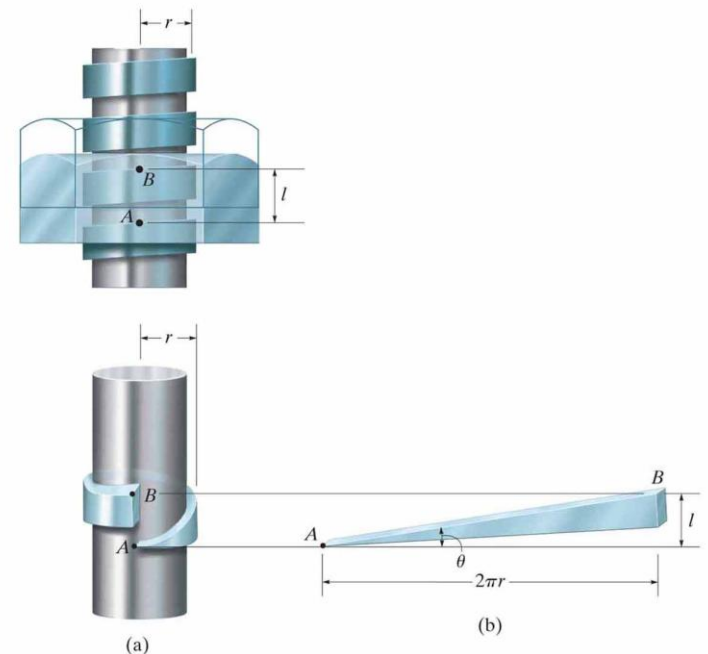


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# Upward Impending Motion

- Consider a square-threaded screw subject to impending motion due to an applied torque  $M$ .
- The free body diagram of the entire unraveled thread through can be represented as follows  
where  $W$  is the vertical force on the or the axial force on the shaft, and  $R$  is the reaction of the groove on the thread.  $R$  has frictional and normal components

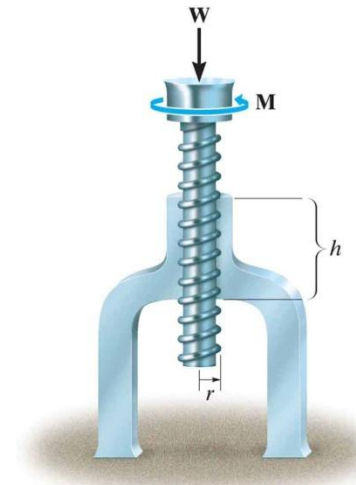
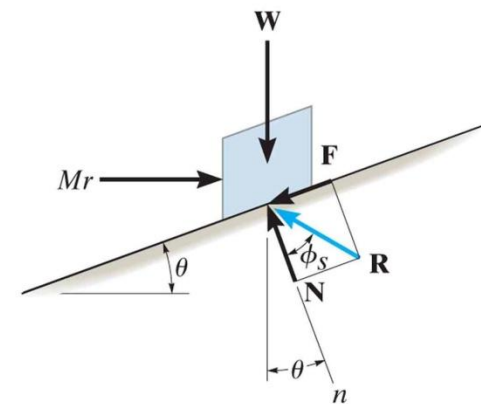


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Upward screw motion  
(a)

fig08\_16a.jpg

# Upward Impending Motion

- The horizontal force associated with the couple moment  $M$  is  $M/r$ .
- The frictional component  $F = \mu_s N$
- The angle of static friction

$$\phi_s = \tan^{-1} \left( \frac{F}{N} \right) = \tan^{-1} \mu_s$$

- By Equations of Equilibrium

$$\rightarrow \sum F_x = 0; \quad \frac{M}{r} - R \sin(\phi_s - \theta) = 0$$

$$\uparrow \sum F_y = 0; \quad R \cos(\phi_s + \theta) - W = 0$$

$$M = rW \tan(\phi_s + \theta)$$

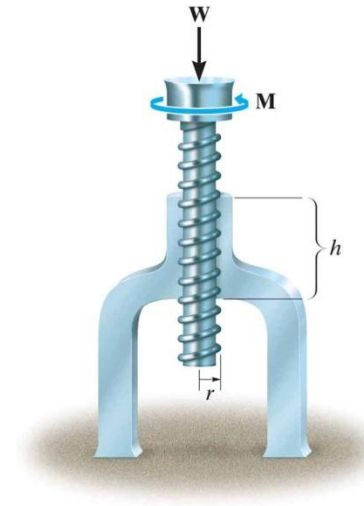
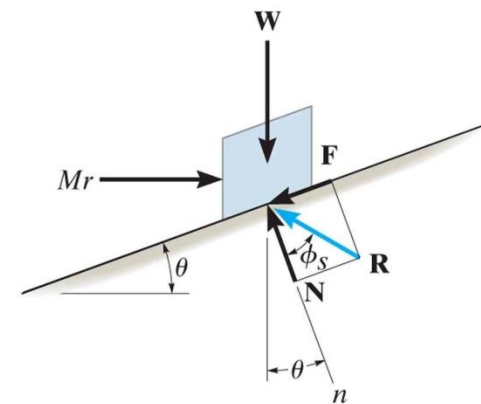


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Upward screw motion  
(a)

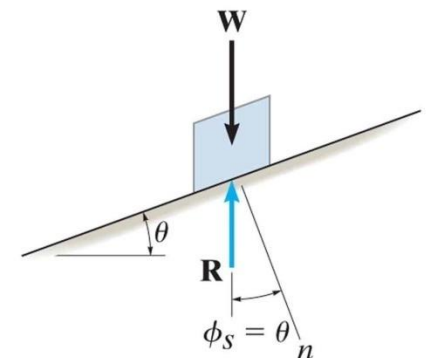
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# Self-Locking Screw

- A screw is *self-locking* if it remains in place under any axial load **W** when the moment **M** is removed.
- In this case **R** acts on the other side of **N**.
- If ,  $\phi_s = \theta$  then **R** will act vertically to balance **W**, and the screw will be on the verge of winding downwards



Self-locking screw ( $\theta = \phi_s$ )  
(on the verge of rotating downward)

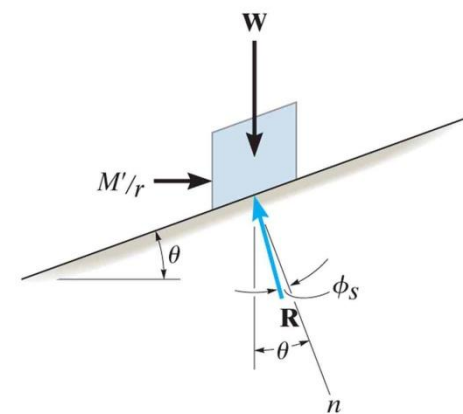
(b)

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# Downward Impending Motion

- If a screw is self-locking, a couple  $\mathbf{M}'$  must be applied in the opposite direction to wind the screw downward
- $\phi_s > \theta$
- This causes a horizontal force in the reverse direction that will push the thread downwards
- Using the previous procedure it can be shown that

$$M' = rW \tan(\theta - \phi_s)$$



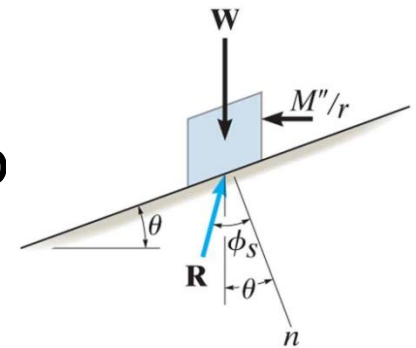
Downward screw motion ( $\theta > \phi_s$ )

(c)

# Downward Impending Motion

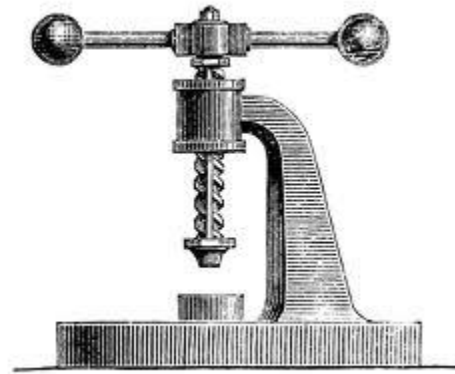
- If the screw is not self-locking it is necessary to apply a moment  $M''$  to prevent the screw from winding downwards
- $\phi_s < \theta$
- A horizontal force  $M''/r$  is required to push against the thread to prevent it from sliding downwards
- The magnitude of the moment required to this unwinding is

$$M'' = rW \tan(\phi_s - \theta)$$



Downward screw motion ( $\theta < \phi_s$ )

(d)



# Pivot & Collar Bearings

- *Pivot* and *collar bearings* are used in machines to support an axial load on a rotating shaft
- In the absence of lubrication, the laws of dry friction may be applied to determine the moment needed to turn the shaft as it supports the axial load.

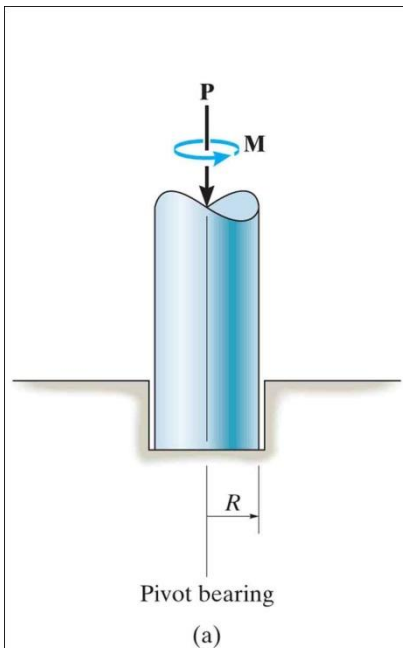


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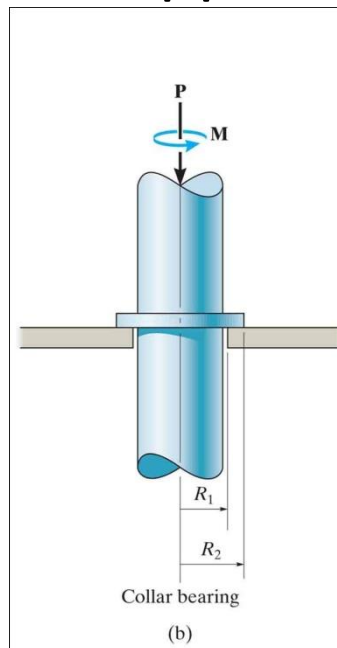


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# Pivot & Collar Bearings: Analysis

- If  $\mathbf{P}$  is the axial force, and the contact area is  $\pi(R_2^2 - R_1^2)$ , then the normal pressure

$$p = \frac{P}{\pi(R_2^2 - R_1^2)}$$

- Consider an infinitesimally small area of collar subjected to normal force  $dN$  and its associated frictional force  $dF$

$$dA = (rd\theta).(dr), \quad dN = p dA$$

$$dF = \mu_s dN = \mu_s p dA = \frac{\mu_s P}{\pi(R_2^2 - R_1^2)} dA$$

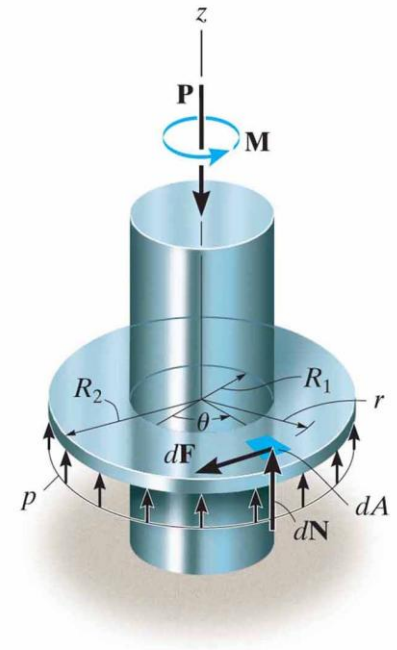


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# Pivot & Collar Bearings: Analysis

- The frictional force creates a moment about the z-axis  $dM = r dF$

- For impending motion

$$\sum M_z = 0; \quad M - \int r dF = 0$$

- Substituting for  $dF$  and  $dA$  and integrating over the entire bearing area

$$M = \int_{R_1}^{R_2} \int_0^{2\pi} r \left[ \frac{\mu_s P}{\pi(R_2^2 - R_1^2)} \right] (r d\theta dr) = \frac{\mu_s P}{\pi(R_2^2 - R_1^2)} \int_{R_1}^{R_2} r^2 dr \int_0^{2\pi} d\theta$$

$$M = \frac{2}{3} \mu_s P \left( \frac{R_2^3 - R_1^3}{R_2^2 - R_1^2} \right)$$

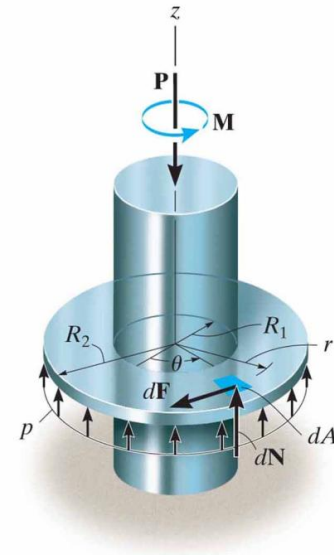


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# Pivot & Collar Bearings: Analysis

- If the shaft is rotating at constant speed, substitute  $\mu_k$  for  $\mu_s$

- For a pivot bearing  $R_2 = R$  and  $R_1 = 0$ , so

$$M = \frac{2}{3} \mu_s PR$$

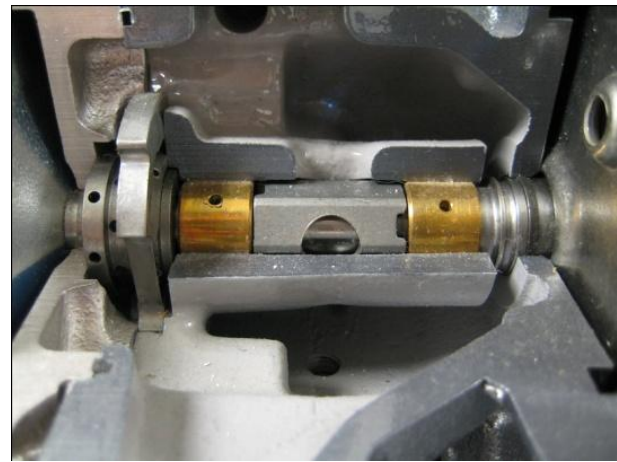
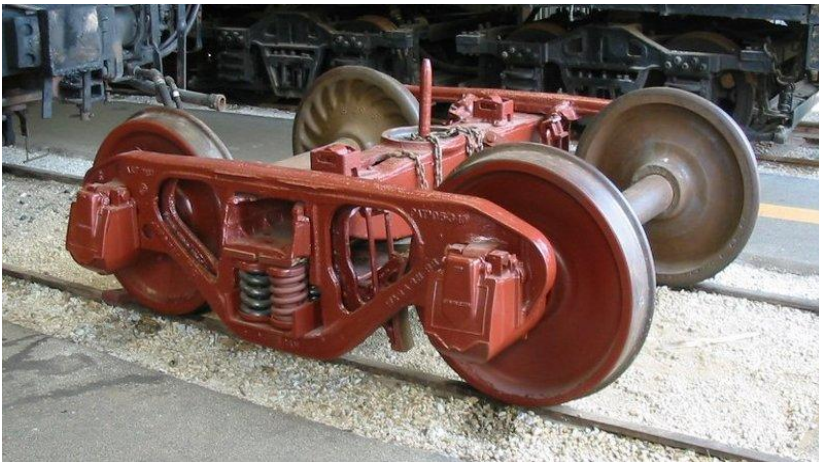
- Note that the above equation are based on constant (uniform) pressure on the bearing surfaces.
- If that is not the case a function relating pressure and bearing area must be determined before integrating





# Journal Bearings

- When a shaft or axle is subjected to lateral loads , a journal bearing is used for support.
- In the absence of lubrication we can apply the laws of dry friction



# Journal Bearings: Analysis

- Consider the journal bearing support shown
- If the shaft is subjected to a vertical force, resulting in a reactive force at A,
- the moment needed to maintain constant rotation about the z-axis can be found from

$$\sum M_z = 0; \quad M - (R \sin \phi_k) r = 0$$

$$M = Rr \sin \phi_k$$

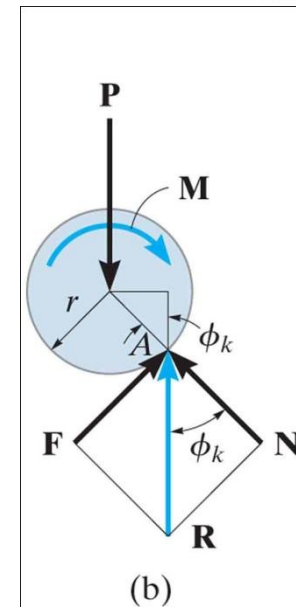
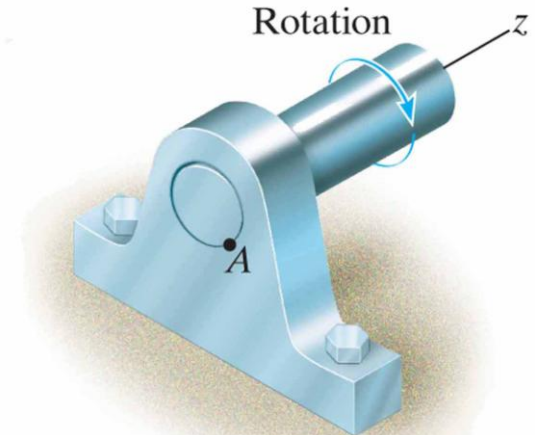


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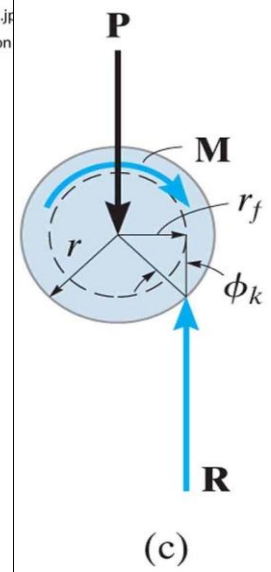


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# Journal Bearings: Analysis

Where  $\phi_s$  is the angle of kinetic friction, and

$$\tan \phi_k = F / N = \mu_k N / N = \mu_k$$

- From diagram it can be seen that

$$r \sin \phi_k = r_f$$

- The dashed circle with radius  $r_f$  is called the friction circle and R will always be tangent to it
- If there is some lubrication  $\sin \phi_k \approx \tan \phi_k \approx \mu_k$
- And the moment needed to overcome the friction becomes

$$M \approx Rr\mu_k$$

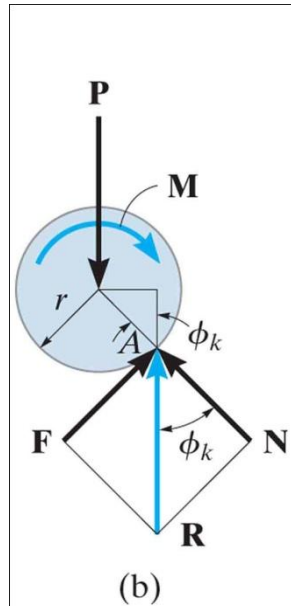


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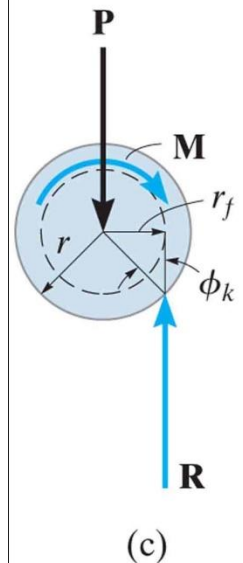


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# Journal Bearings: Analysis

- In practice journals are prone to rapid wear due to friction between shaft and bearing.
- In engineering design this is overcome by incorporating ball bearings or rollers in the journal bearing to reduce frictional losses





# Rolling Resistance

- Consider a *rigid* cylinder rolling at constant velocity over a *rigid* surface.
- Now if the rigid cylinder rolls over a softer surface, it deforms the material of the surface in front of it.
- The reaction of the surface on the cylinder retards its forward motion.
- The material at the rear of the cylinder however rebounds and pushes the cylinder forward

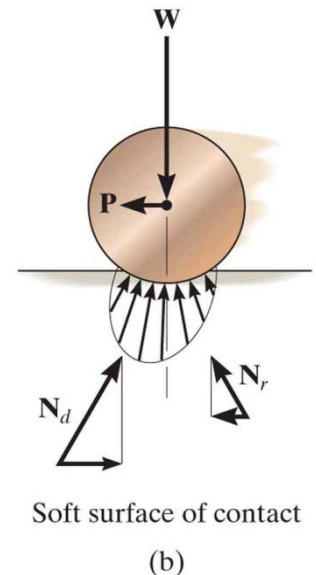
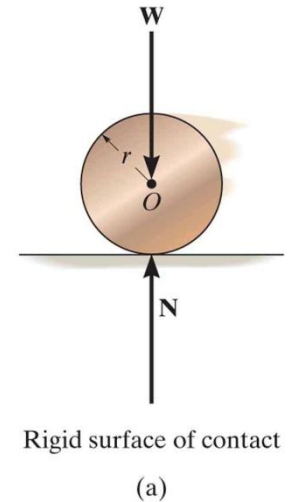


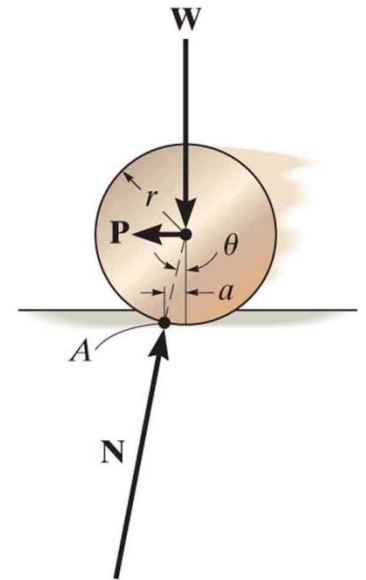
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# Rolling Resistance

- The deformation force always exceeds the restoration/ rebound force, hence the resistance to rolling.
- The force required to maintain the motion at that constant velocity is

$$P \approx \frac{Wa}{r}$$

where  $a$  is the coefficient of rolling resistance



(d)

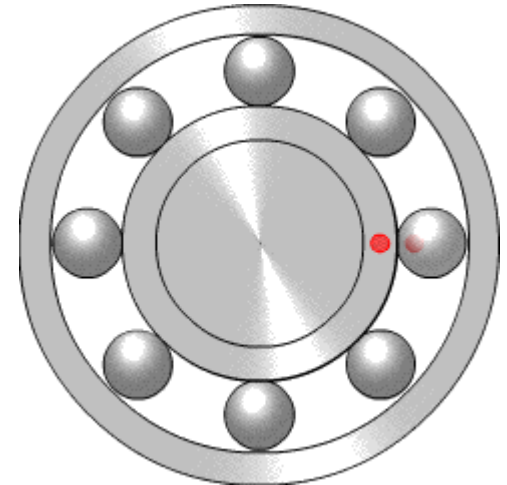
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# Rolling Resistance

- Rolling resistance is significantly lower than sliding resistance
- Also for a given body, the harder the surface the less the rolling resistance
- The above explain why rollers or ball bearings can be used to minimize friction between moving part of machines



# Comments & Questions

